

# **Thermal-hydraulic instability**

# Definition of thermal-hydraulic instability

*Periodic or multiple change in thermal-hydraulic parameters of the flow in separate channels or in circulation loop at stationary operating conditions of the setup is known as **flow instability**.*

# Types of instabilities

Type	Manifestation pattern	Cause
Main static instability (Ledinegg type)	Sudden change in flow rate towards a new steady value	Different pattern of the ratio $\Delta P = f(G)$
Complex dynamic instability (turn-to-turn pulsation)	Redistribution of flow rates in parallel channels	Interaction of $G$ , $x$ , $\Delta P$
Complex dynamic instability (general pulsation in evaporator)	Periodic change in total flow rate in the circuit	Unstable operation of the 'heat exchanger-pump' system

# Main static instability (Ledinegg type)

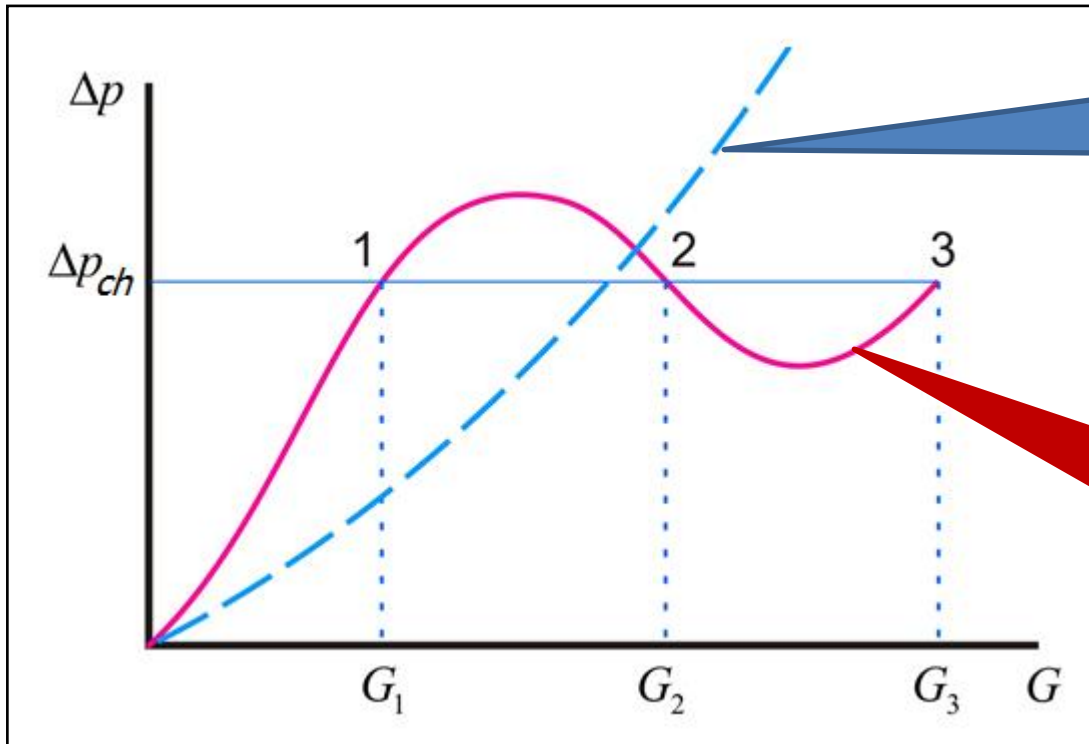
Disturbance of uniform distribution of the fluid in parallel channels (tubes) may be caused by 2 reasons:

- hydraulic non-uniformity  $\eta_H \neq 1$ ;
- ambiguity of the channel's hydrodynamic characteristics (HDC)

$$\Delta p_{ch} = f(G)$$

$$\Delta p_{ch} = p_{in} - p_{out}$$

# Static hydraulic characteristics of channel



Unambiguous HDC:  
one value of  $\Delta p_{ch}$  – one flow  
rate  $G$

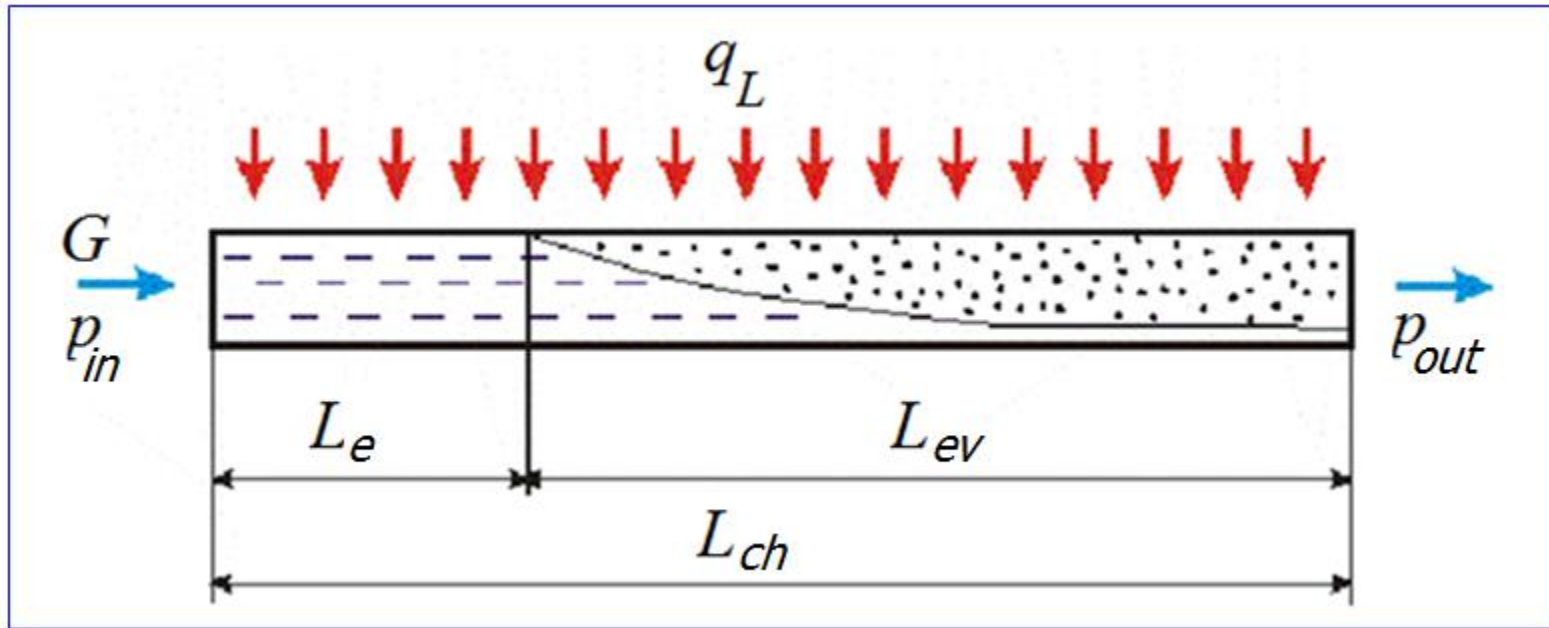
Ambiguous HDC:  
one value of  $\Delta p_{ch}$  – three  
flow rates  $G_1, G_2, G_3$

Here  $\Delta p_{ch} = p_{in} - p_{out}$  – pressure differential in the channel;  
 $p_{in}, p_{out}$  – channel inlet and outlet pressures;  
 $G$  - mass flow rate

# Factors that affect flow instability

1. Subcooling to saturation at the inlet  $\Delta h_3$
2. Flow direction (upstream, downstream)
3. Pressure
4. Local resistances

# Schematic of a steam-generating tube (channel)



Here  $q_L$  - linear heat flux, W/m;

$L_{ch}$  - channel length, m;

$L_e$ ,  $L_{ev}$  - length of economizing and evaporation zones, m;

$p_{in}$ ,  $p_{out}$  - pressure at the channel inlet and outlet

# Derivation of HDC equation

Main assumptions:

- ❖ steam-generating channel consists of economizing and evaporation zones;
- ❖ linear heat flux  $q_L = \text{const}$ ;
- ❖ specific volume in evaporation zone is equal to specific volume of saturated water  $v_{ev} = v'$

Here **HDC** is hydrodynamic characteristics of the channel

$$\Delta p_{ch} = f(G)$$

$$\Delta p_{ch} = P_{in} - P_{out}$$



## Derivation of HDC equation

$$\Delta p_{ch} = \Delta p_e + \Delta p_{ev}$$

$$\Delta p_{ch} = \xi \cdot \frac{L_e}{d_{ch}} \cdot \frac{G^2 \cdot v'}{2 \cdot f_{ch}^2} + \xi \cdot \frac{L_{ch} - L_e}{d_{ch}} \cdot \frac{G^2 \cdot v_{mix}}{2 \cdot f_{ch}^2}$$

Additional ratios:

$$f_{ch} = \frac{\pi \cdot d_{ch}^2}{4} \quad w = \frac{G}{f_{ch} \cdot \rho} \quad \Delta p = \xi \cdot \frac{L}{d_{ch}} \cdot \frac{\rho \cdot w^2}{2}$$

## Derivation of HDC equation

$$L_e = \frac{G \cdot (h' - h_{in})}{q_L} = \frac{G \cdot \Delta h_{in}}{q_L}$$

$$v_{mix} = \frac{v' + x \cdot (v'' - v')}{2}$$

$$x = \frac{q_L \cdot (L_{ch} - L_e)}{G \cdot (h'' - h')}$$

## HDC equation

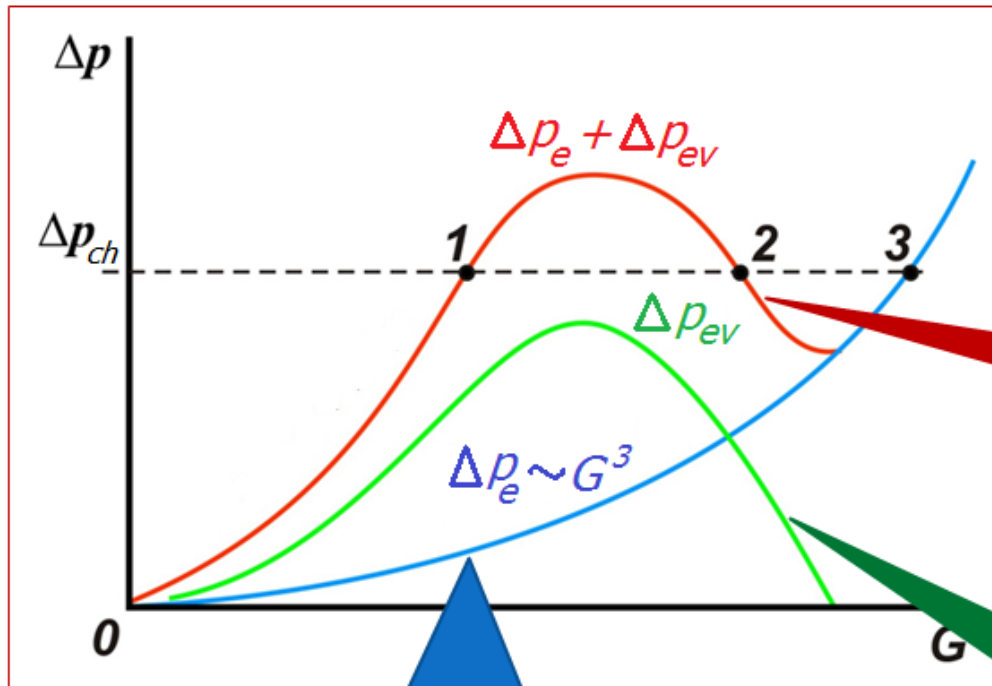
$$\Delta p_{ch} = A \cdot G^3 - B \cdot G^2 + C \cdot G$$

$$A = \frac{\xi \cdot (v'' - v') \cdot 2 \cdot \Delta h_{in}^2}{4 \cdot f_{ch}^2 \cdot d_{ch} \cdot q_L \cdot r}$$

$$B = \frac{\xi \cdot L_{ch}}{2 \cdot f_{ch} \cdot d_{ch}} \cdot \left[ \frac{\Delta h_{in}}{r} \cdot (v'' - v') - v' \right]$$

$$C = \frac{\xi \cdot (v'' - v') \cdot L_{ch}^2 \cdot q_L}{4 \cdot f_{ch}^2 \cdot d_{ch} \cdot r}$$

# Physical causes of non-uniformity



Pressure differential in the channel

Pressure differential in the economizer zone

Pressure differential in the evaporation zone

# Physical causes of non-uniformity

The emergence of non-uniformity is explained by the effect of zone lengths  $L_e$  and  $L_{ev}$ :

- ❖ length of the economizer zone  $L_e$  rises proportionally with an increasing flow rate  $G$ ;
- ❖ on the other hand, increasing flow rate  $G$  results in decreasing length of the evaporation zone  $L_{ev}$ .

Thus, resistance of the evaporation zone  $\Delta p_{ev}$  depends on medium flow rate  $G$  in a *complex* way. All this leads to ambiguity of the channel's static hydraulic characteristics.

## Condition for HDC unambiguity

$$\left(\frac{\Delta h_{in}}{r}\right) \cdot (\rho' / \rho'' - 1) \leq B$$

- at  $B > 7.5$  – **ambiguous** HDC;
- at  $B \approx 7.5$  – **unambiguous** HDC, but with plateau;
- at  $B \leq 5$  – **unambiguous** HDC that fulfill the requirement for hydrodynamic stability

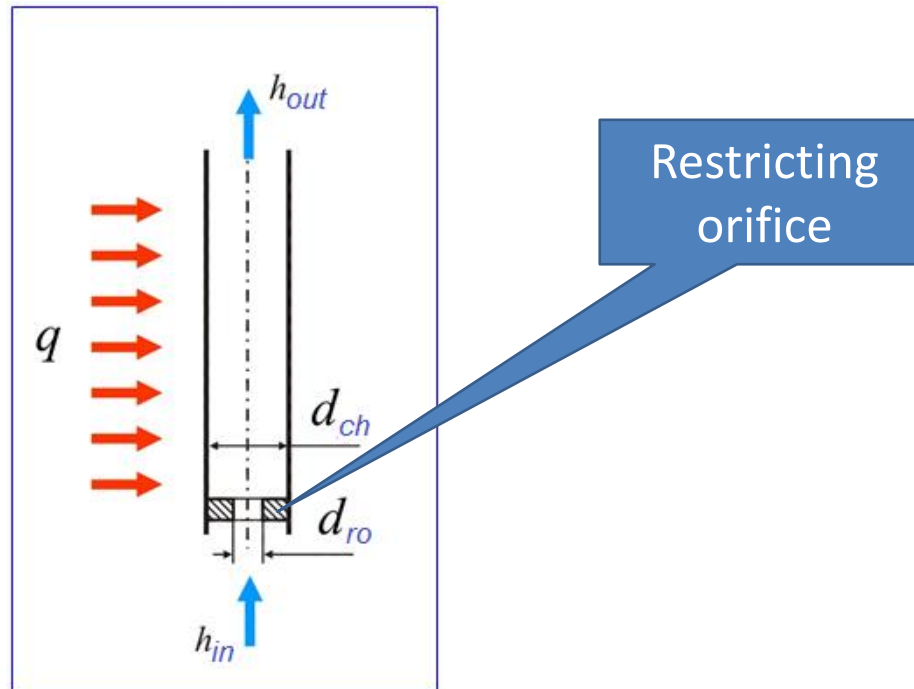
Here  $\Delta h_{in}$  - medium subcooling to saturation temperature;

$r = h'' - h'$  – latent evaporation heat;

$\rho'$ ,  $\rho''$  – density of saturated water and steam

# Practical measures to fight instability

*The main method for the prevention of thermal maldistribution is to install orifices for all inlet regions of the channels*



Thank you for attention